

Cooperative Manipulation via Internal-Force Regulation: A Rigidity Theory Perspective

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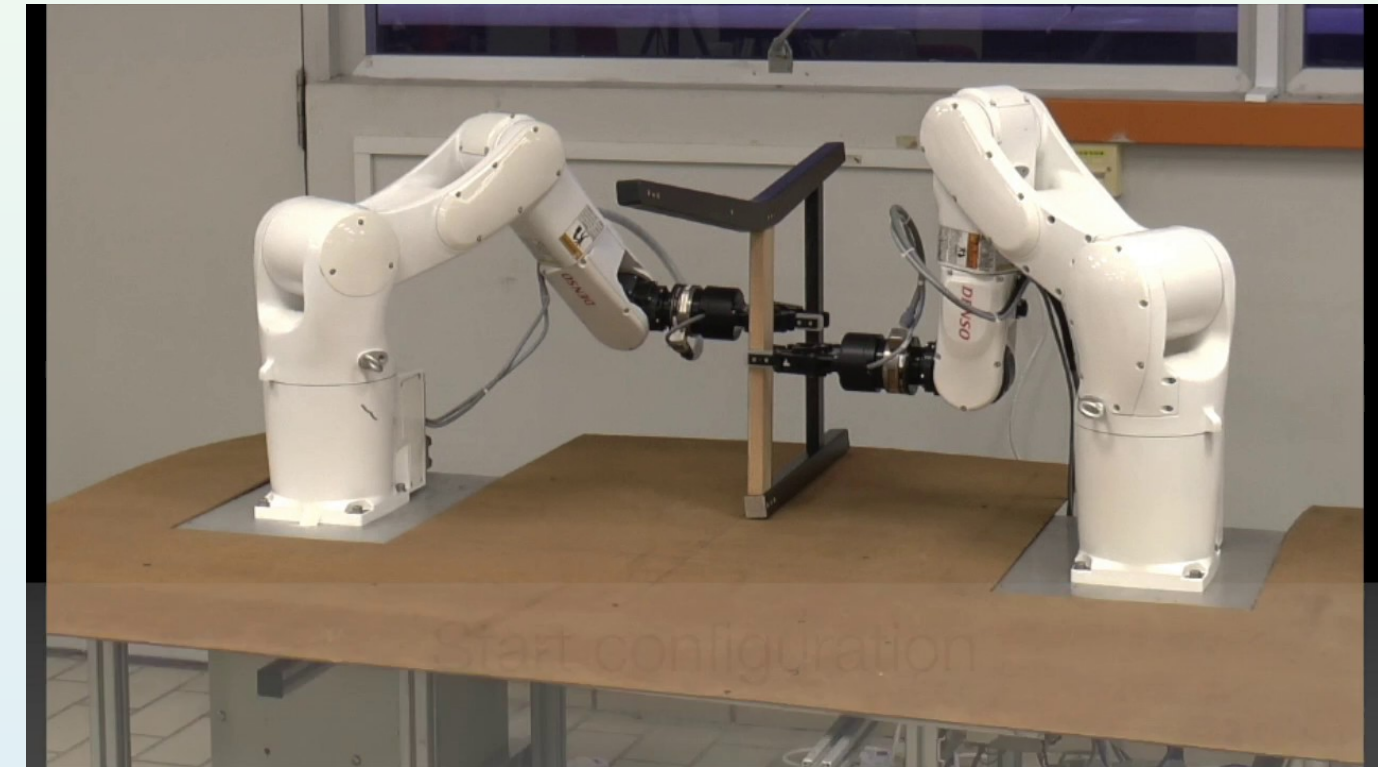
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Motivation

Cooperative manipulation

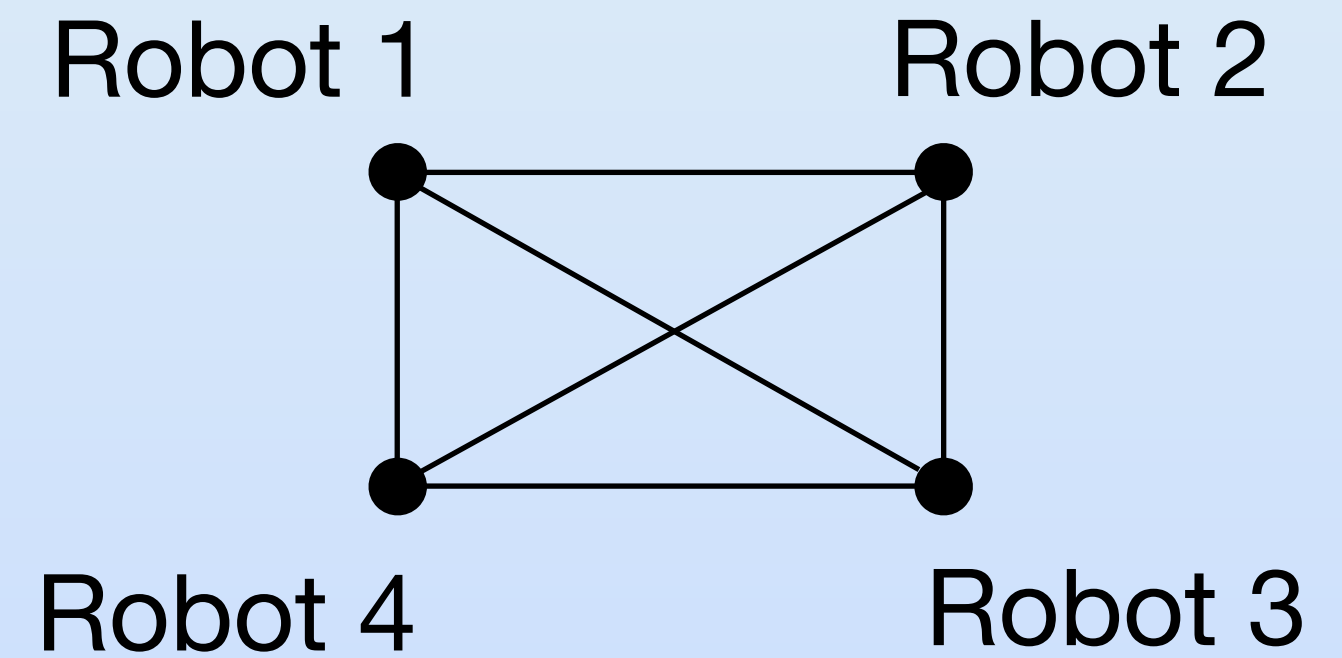
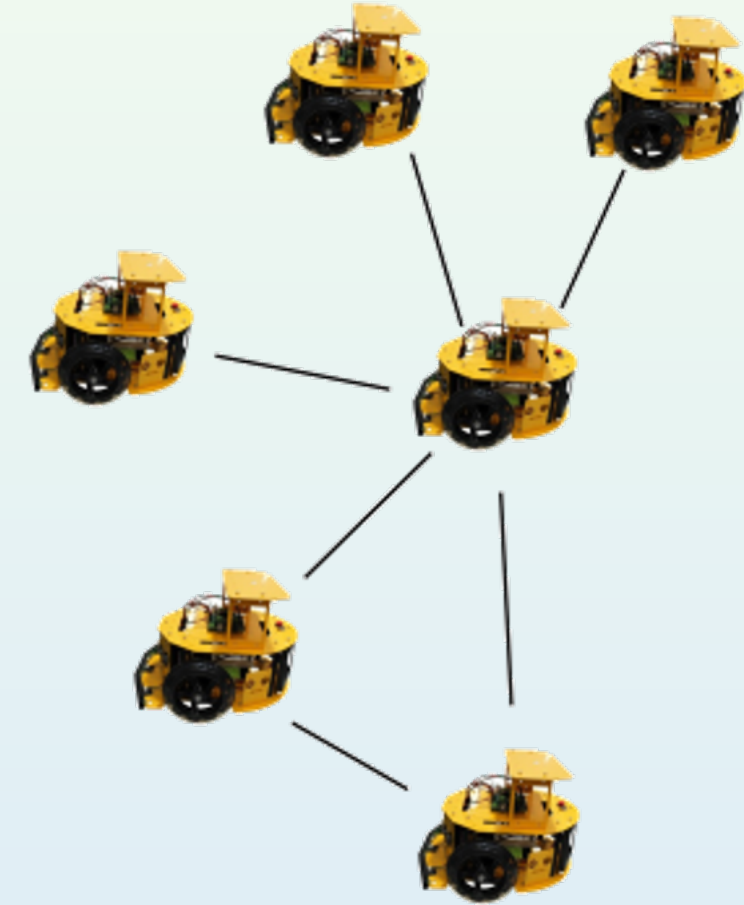
- Large/Heavy payloads
- Challenging manoeuvres
- Bimanual tasks



Motivation

Rigidity theory

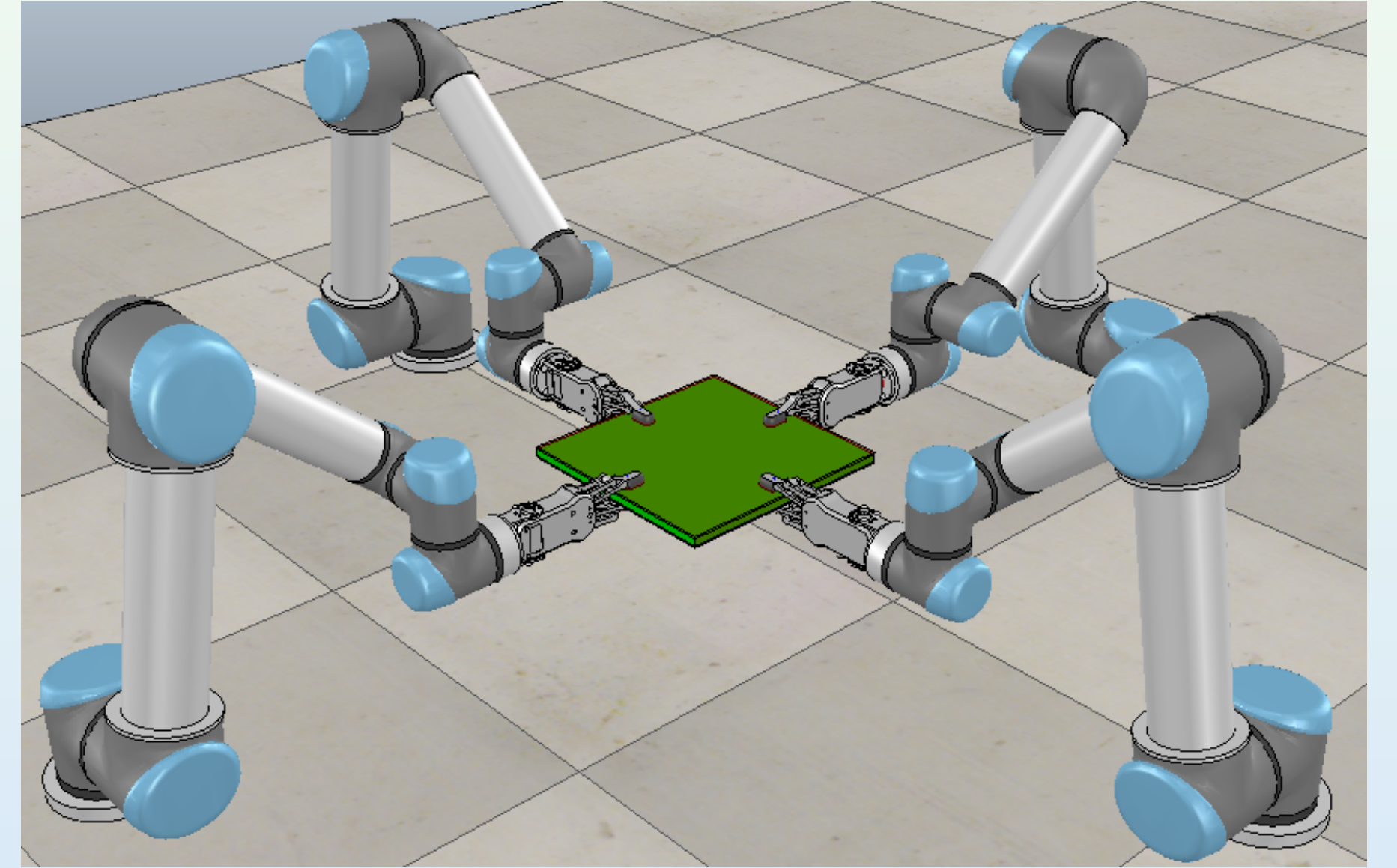
- Understand relations in multi-agent networks
- Formation control
- Distance rigidity, bearing/angle rigidity



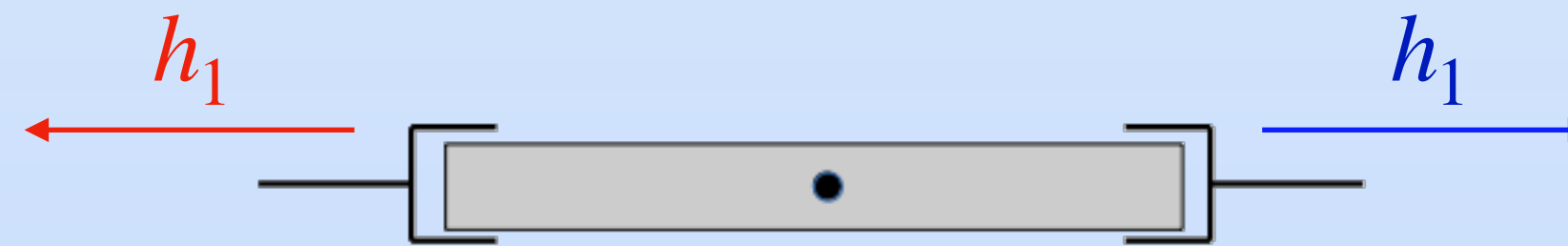
Motivation

Rigid cooperative manipulation

- A group of robots grasp an object *rigidly*
- Aim to achieve trajectory tracking by object's COM
- How do we *minimize internal forces*?

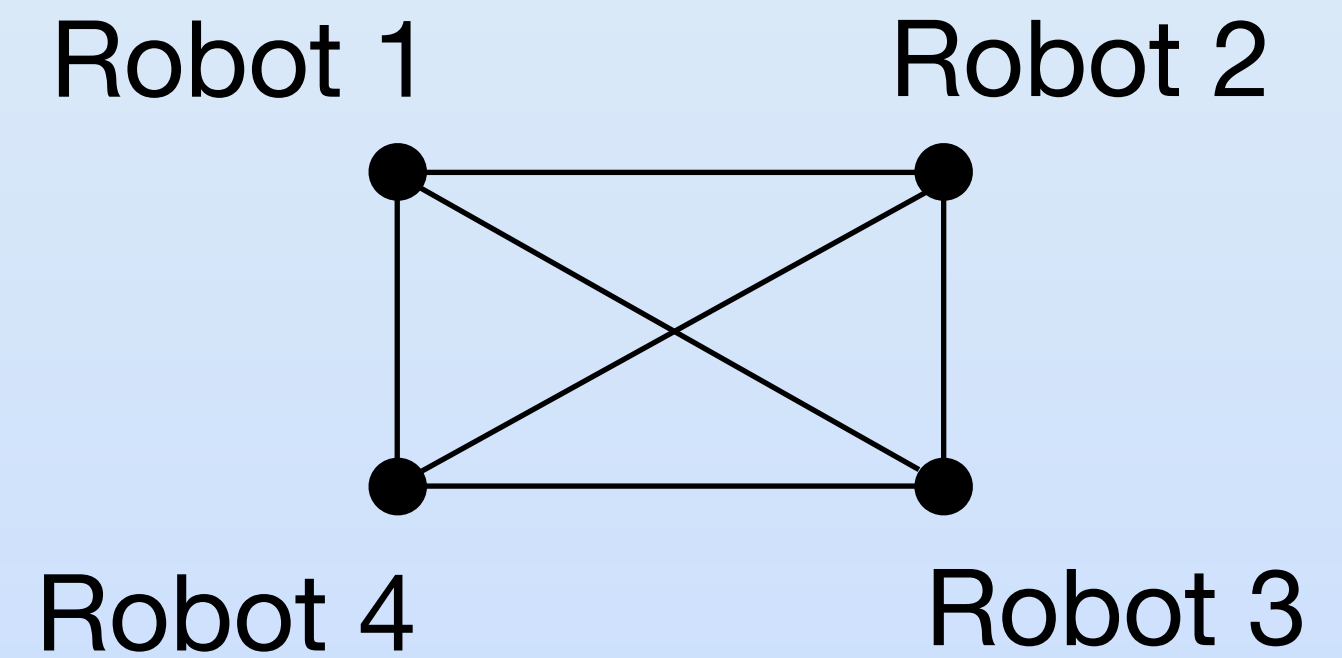
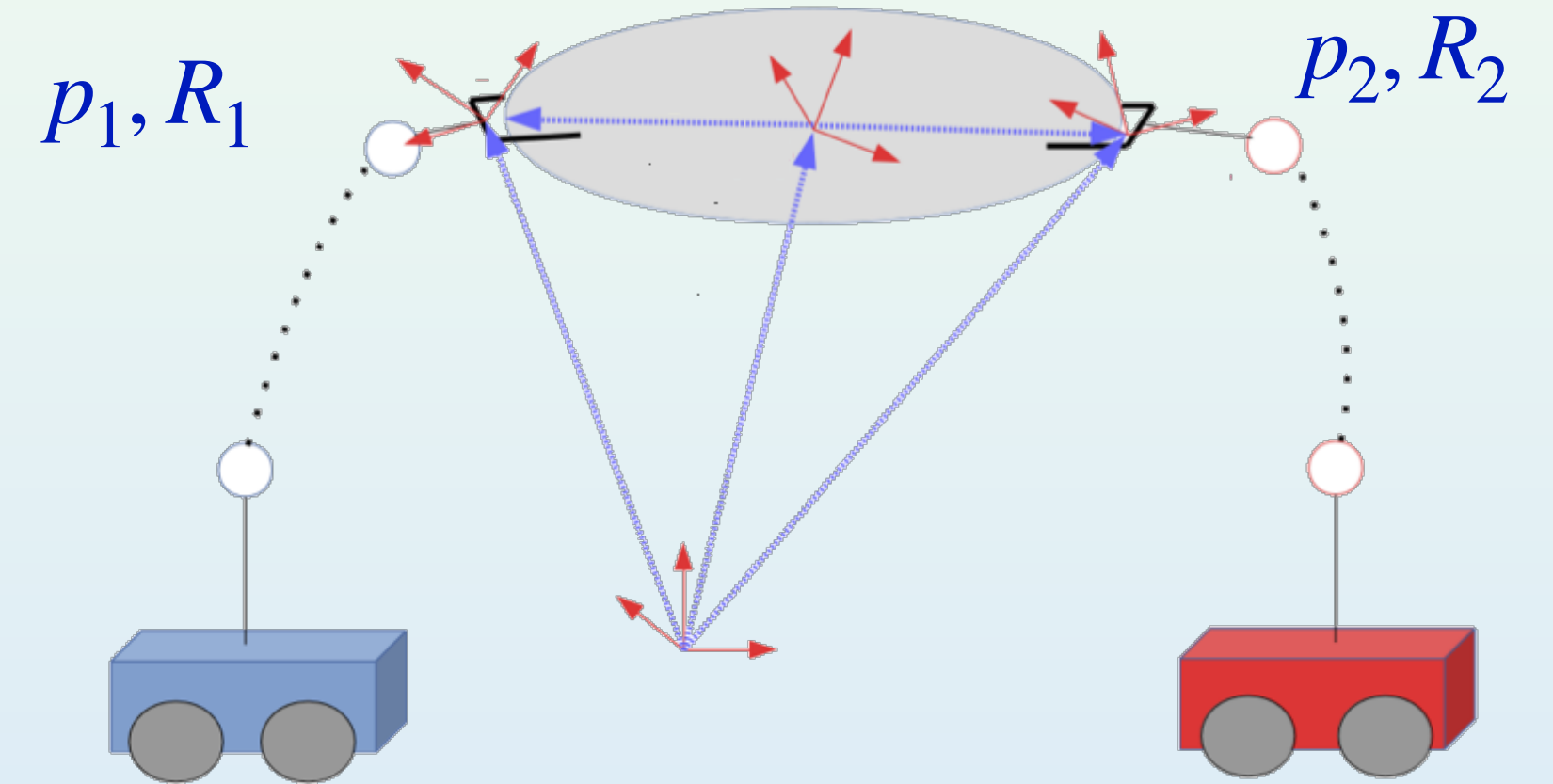


Internal forces: forces produced by the agents that do not contribute to the object's motion



Distance and bearing rigidity in SE(3)

- Characterise motions that preserve *distances* and *bearings* between agents $\mathcal{N} = \{1, \dots, N\}$
- Multi-agent network:
 - Directed graph: $\mathcal{E} \subseteq \{(i, j) \in \mathcal{N} : i \neq j\}$
 - Undirected graph: $\mathcal{E}_u = \{(i, j) \in \mathcal{E} : i < j\}$
- Distance and bearing constraints:
 - Distance: $\gamma_{e,d} = \frac{1}{2} \|p_i - p_j\|^2, e \in \mathcal{E}_u$
 - Bearing: $\gamma_{e,b} = R_i^\top \frac{p_i - p_j}{\|p_i - p_j\|}, e \in \mathcal{E}$
 - D&B function: $\gamma_{\mathcal{E}} = [\gamma_{1,d}, \dots, \gamma_{|\mathcal{E}_u|,d}, \gamma_{1,b}^\top, \dots, \gamma_{1,|\mathcal{E}|}^\top]^\top$

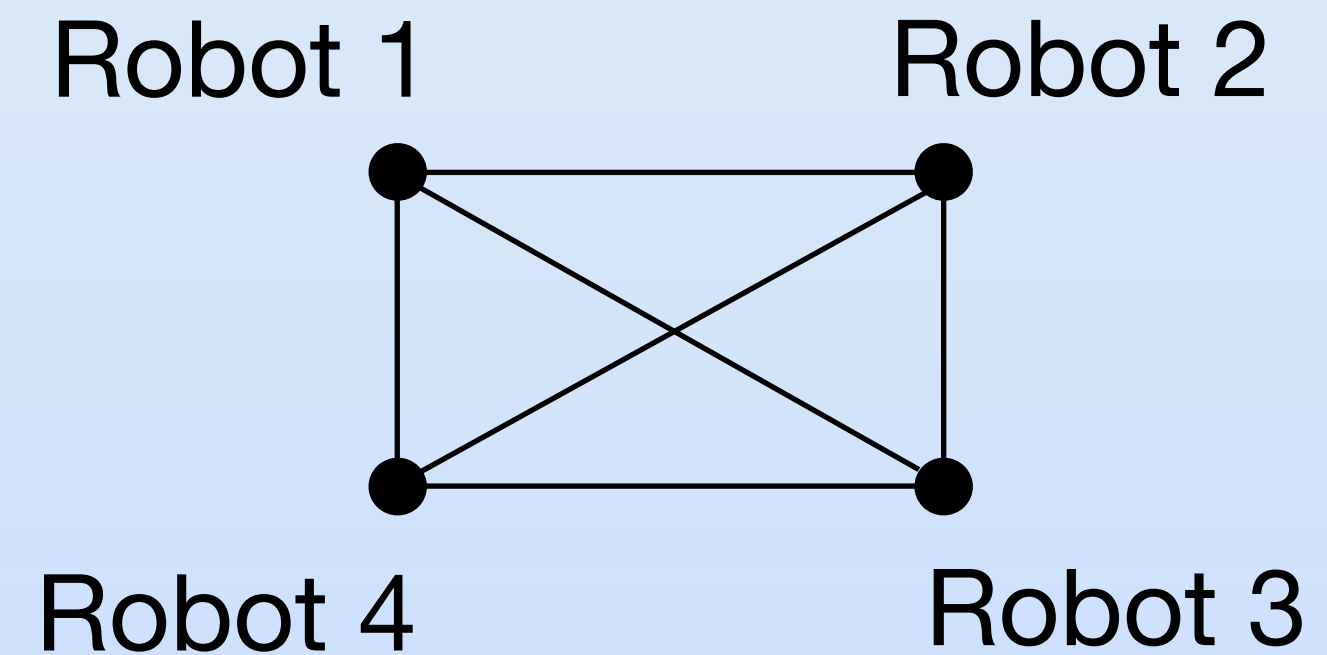
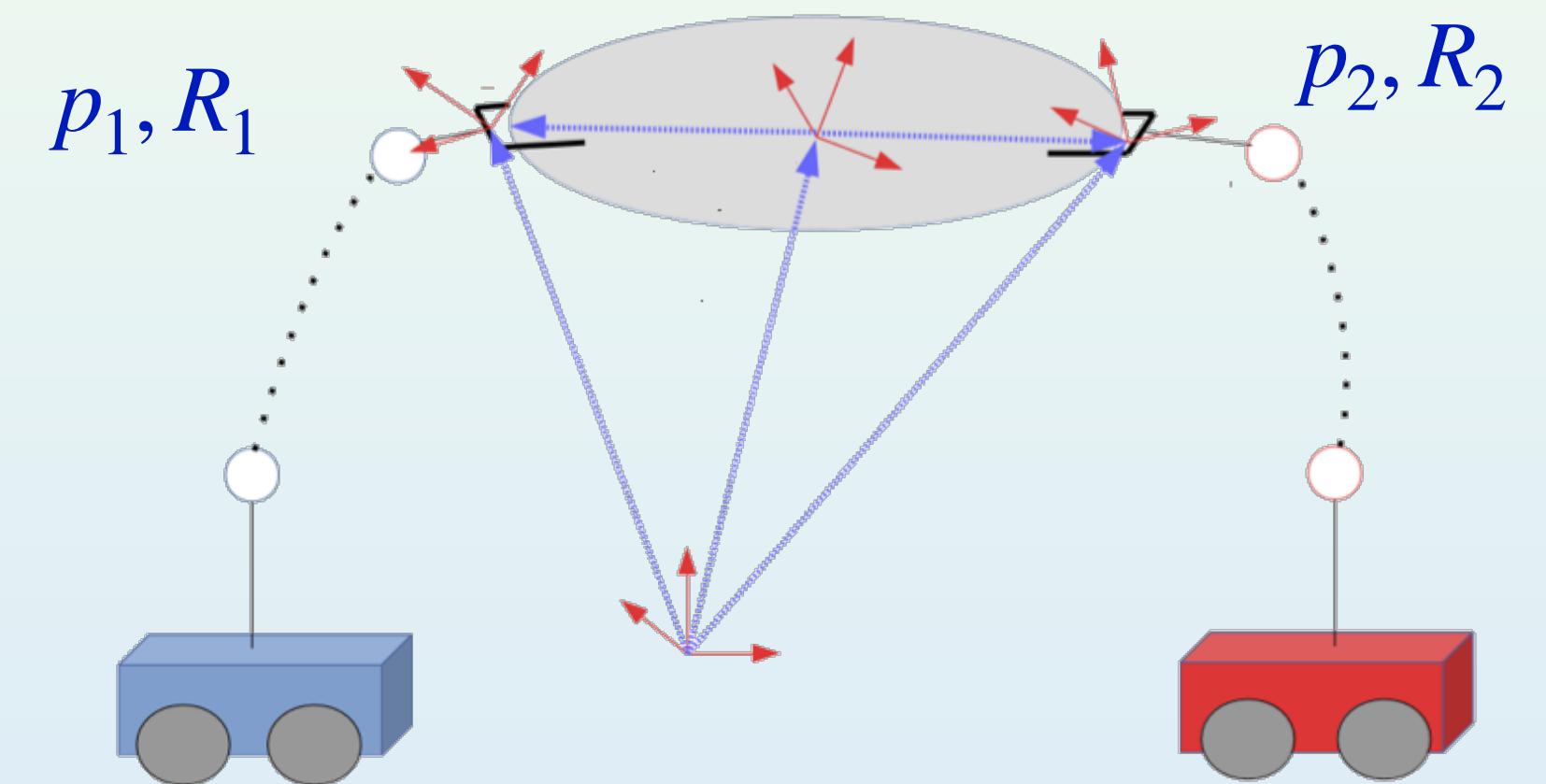


Infinitesimal distance and bearing rigidity in SE(3)

Infinitesimal motions: motion-perturbations of the agents that leave the rigidity function $\gamma_{\mathcal{E}}$ unchanged

Rigidity matrix

$$\mathcal{R}_{\mathcal{E}}(x) = \begin{bmatrix} \frac{\partial \gamma_{\mathcal{E}}}{\partial p_1} & \frac{\partial \gamma_{\mathcal{E}}}{\partial R_1} & \cdots & \frac{\partial \gamma_{\mathcal{E}}}{\partial p_N} & \frac{\partial \gamma_{\mathcal{E}}}{\partial R_N} \end{bmatrix}$$



Infinitesimal motions: motions $x(t)$ produced by the nullspace of $\mathcal{R}_{\mathcal{E}}(x)$, i.e.,

$$\dot{\gamma}_{\mathcal{E}} = \mathcal{R}_{\mathcal{E}}(x(t))\dot{x}(t) = 0$$

Trivial motions: motions that preserve the distances and bearings of the system

D&B infinitesimally rigid system:
infinitesimal motions are trivial motions

Infinitesimal distance and bearing rigidity in SE(3)

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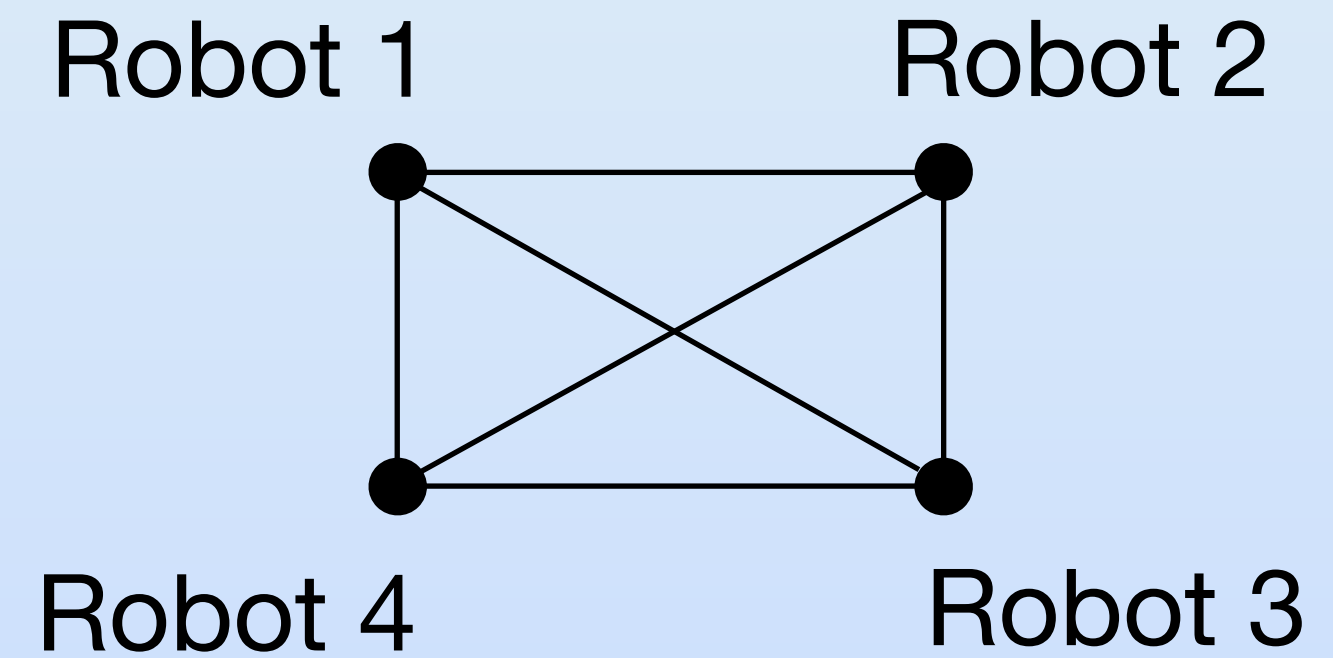
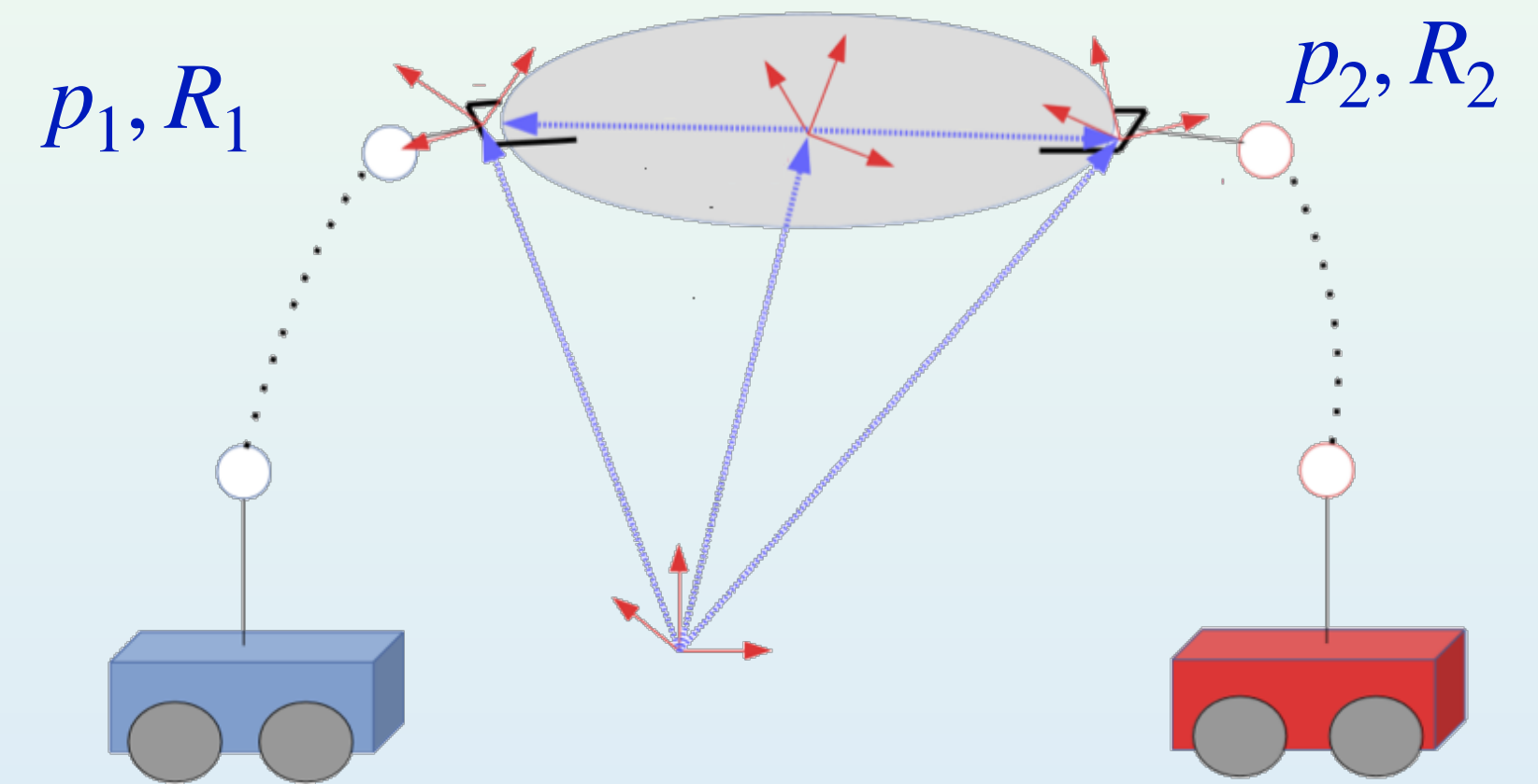
The multi-agent system is D&B infinitesimally rigid in SE(3) if and only if

$$\text{rank}(\tilde{\mathcal{R}}_{\mathcal{E}}) = 6N - 6$$

where

$$\tilde{\mathcal{R}}_{\mathcal{E}}(x) = \begin{bmatrix} \frac{\partial \gamma_{\mathcal{E}}}{\partial p_1} & \cdots & \frac{\partial \gamma_{\mathcal{E}}}{\partial p_N} & \frac{\partial \gamma_{\mathcal{E}}}{\partial R_1} & \cdots & \frac{\partial \gamma_{\mathcal{E}}}{\partial R_N} \end{bmatrix}$$

is a column-permutation of $\mathcal{R}_{\mathcal{E}}$



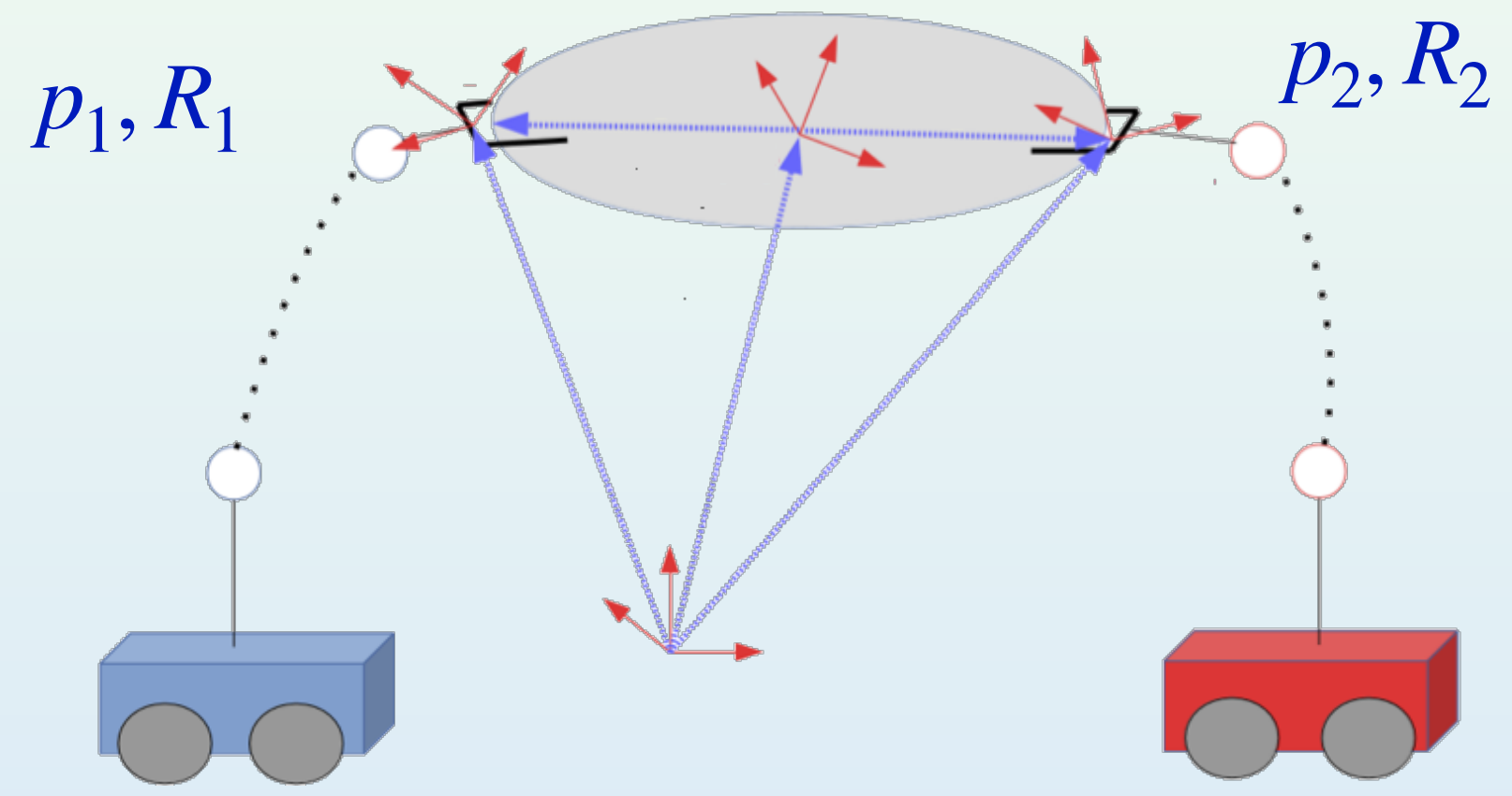
Cooperative manipulation modelling

- Robot dynamics

$$\begin{cases} v = [\dot{p}_1^\top, \omega_1^\top, \dots, \dot{p}_N^\top, \omega_N^\top]^\top \\ \dot{R}_i = S(\omega_i)R_i \\ M(x)\dot{v} + C(x, \dot{x})v + g(x) = u - h \end{cases}$$
- Object dynamics

$$\begin{cases} v_o = [\dot{p}_o^\top, \omega_o^\top]^\top \\ \dot{R}_o = S(\omega_o)R_o \\ M_o(x)\dot{v}_o + C(x_o, \dot{x}_o)v_o + g_o(x) = h_o \end{cases}$$

Skew-symmetric matrix



- Object-robots coupling:

- Velocities: $v = G(x)^\top v_o$
- Forces: $h_o = G(x)h$

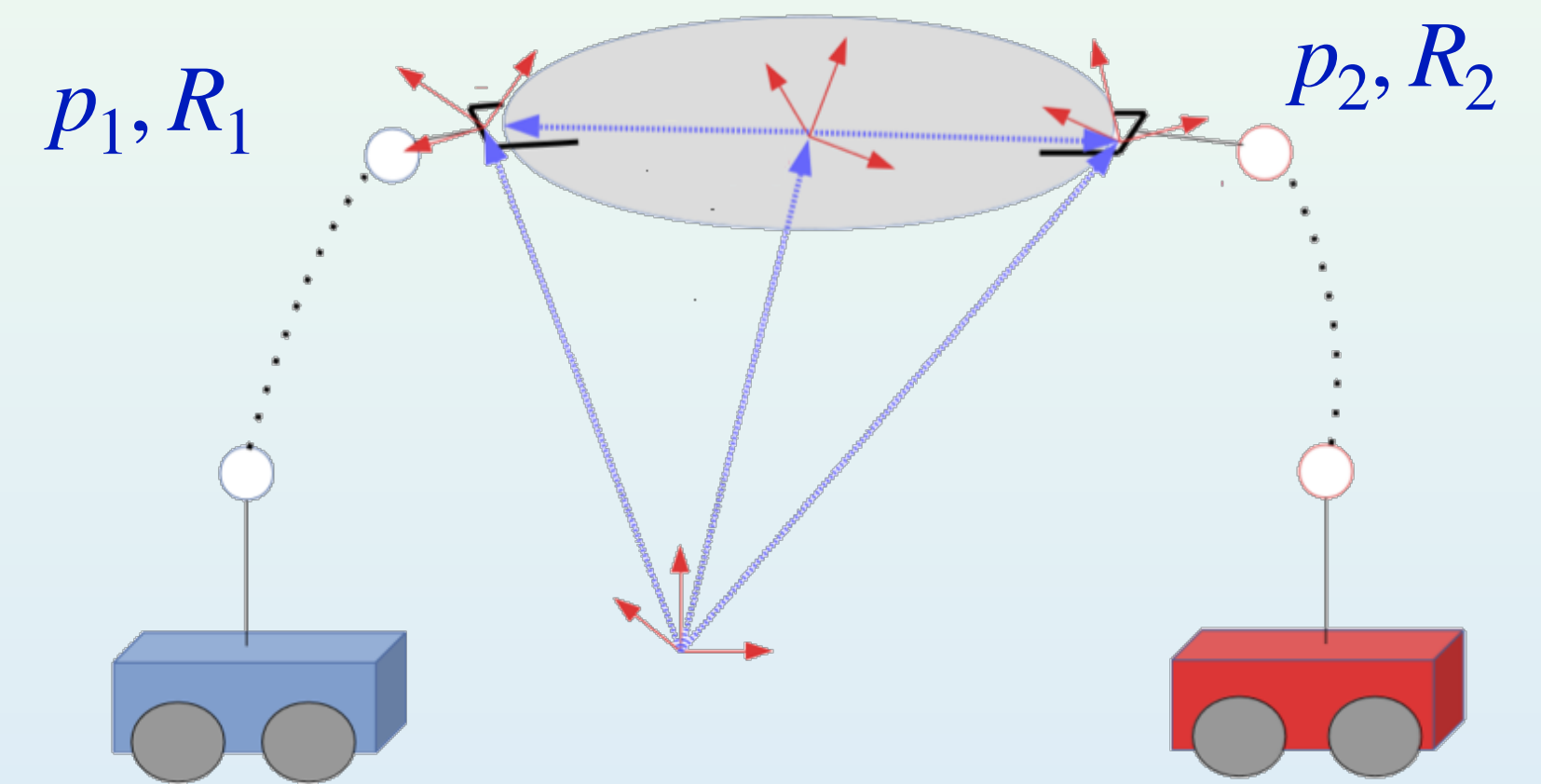
Grasp matrix: $G(x) = [J_{o_1}(x_1)^\top, \dots, J_{o_N}(x_N)^\top] \in \mathbb{R}^{6 \times 6N}$

$$J_{o_i}(x_i) = \begin{bmatrix} I_3 & -S(p_i - p_o) \\ 0_{3 \times 3} & I_3 \end{bmatrix}, i \in \mathcal{N}$$

- Force decomposition: $h = h_m + h_{int}$
 - motion-inducing forces (green arrow pointing to h_m)
 - internal forces (red arrow pointing to h_{int}) $(G(x)h_{int} = 0)$

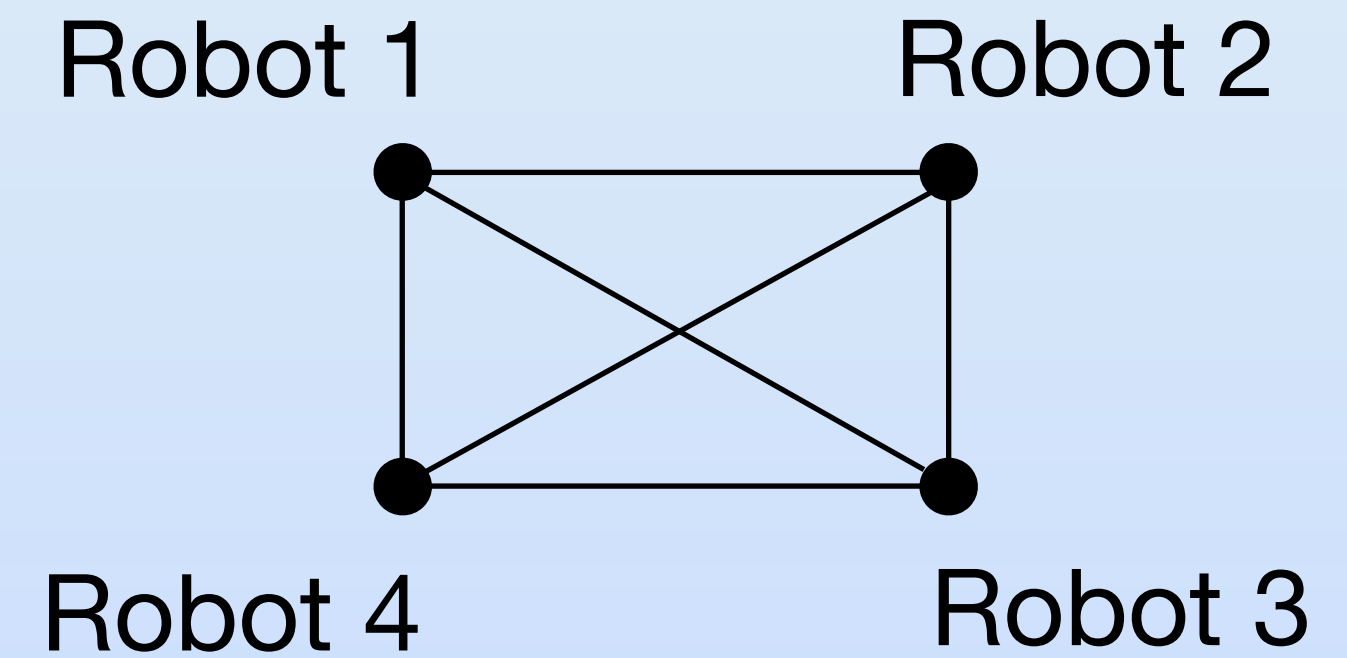
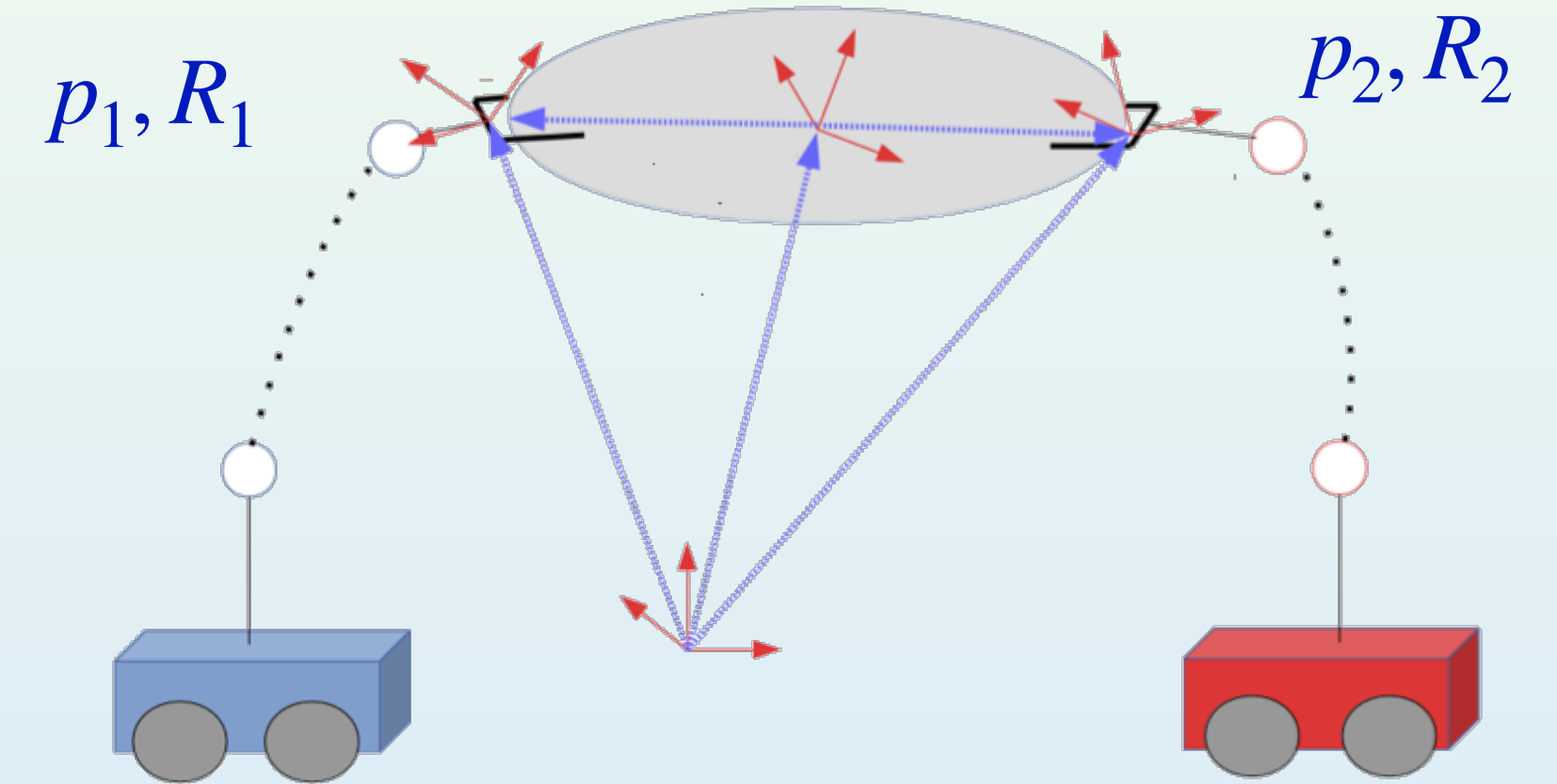
Internal forces based on the D&B rigidity matrix

- View the cooperative manipulation as a graph
 - Interactions among all agents \longrightarrow *complete graph*



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 - Bearing: $\gamma_{e,b} = R_i^\top \frac{p_i - p_j}{\|p_i - p_j\|}, e \in \mathcal{E}$
 - D&B function: $\gamma_{\mathcal{E}} = [\gamma_{1,d}, \dots, \gamma_{|\mathcal{E}_u|,d}, \gamma_{1,b}^\top, \dots, \gamma_{1,|\mathcal{E}|}^\top]^\top$



Internal forces based on the D&B rigidity matrix

- View the cooperative manipulation as a graph
 - Interactions among all agents \longrightarrow *complete graph*

- Cooperative manipulation rigidity constraints: $\gamma_{\mathcal{E}} = 0$
 $\Rightarrow \mathcal{R}_{\mathcal{E}}\dot{v} = -\dot{\mathcal{R}}_{\mathcal{E}}(x)v$

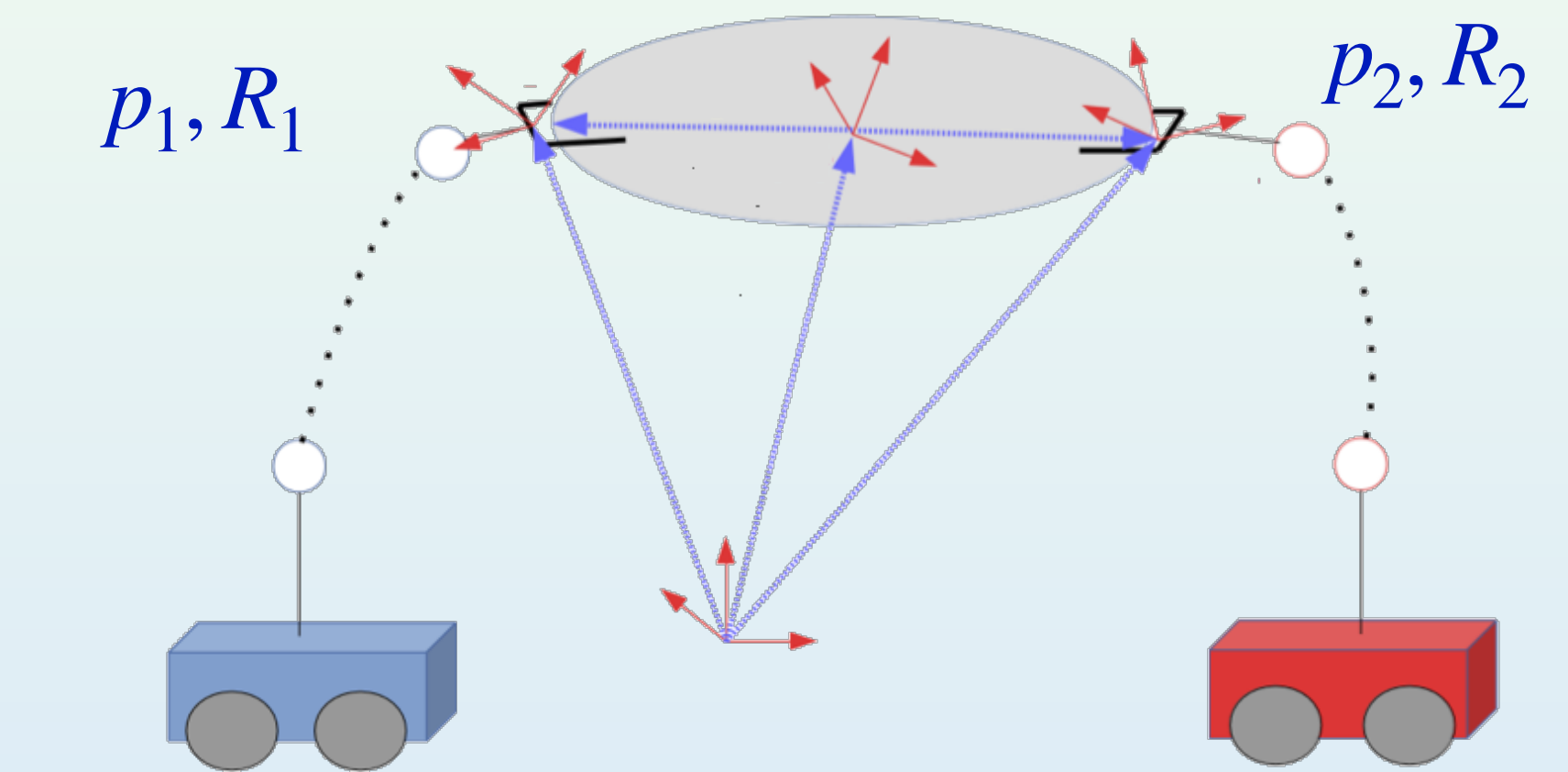
- Complete graph: $\mathcal{R}_{\mathcal{E}}$ encodes rigid body motions

- Internal-force dynamics: $M(x)\dot{v} + C(x, \dot{x})v + g(x) = u - h_{int}$

- Unconstrained dynamics: $M(x)\alpha + C(x, \dot{x})v + g(x) = u$

- Gauss' principle:

$$\begin{aligned} \dot{v} = \min & (\dot{v} - a)^{\top} M(x) (\dot{v} - a) \\ \text{s.t. } & \mathcal{R}_{\mathcal{E}}\dot{v} = -\dot{\mathcal{R}}_{\mathcal{E}}v \end{aligned}$$



Internal forces:

$$h_{int} = M^{\frac{1}{2}}(\mathcal{R}_{\mathcal{E}}M^{-\frac{1}{2}})(\dot{\mathcal{R}}_{\mathcal{E}}v + \mathcal{R}_{\mathcal{E}}a)$$

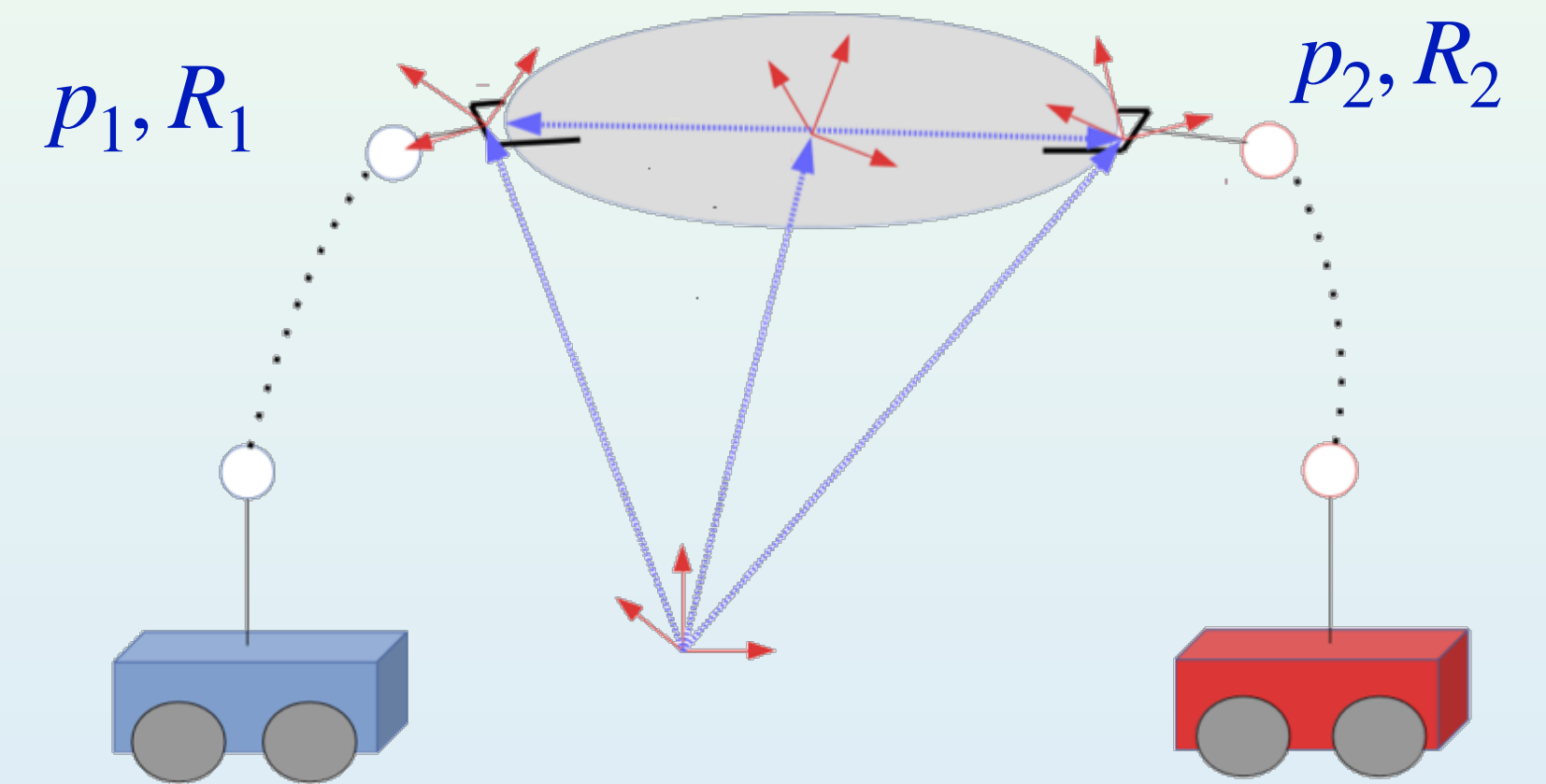
Internal forces based on the D&B rigidity matrix

Internal forces:
$$\begin{cases} h_{int} = M^{\frac{1}{2}}(\mathcal{R}_{\mathcal{G}}M^{-\frac{1}{2}})(\dot{\mathcal{R}}_{\mathcal{G}}v + \mathcal{R}_{\mathcal{G}}a) \\ \alpha = M(x)^{-1}(u - C(x, \dot{x})v + g(x)) \end{cases}$$

Let $\mathcal{R}_{\mathcal{G},1}$ and $\mathcal{R}_{\mathcal{G},2}$ such that $\text{null}(\mathcal{R}_{\mathcal{G},1}) = \text{null}(\mathcal{R}_{\mathcal{G},2})$
and let

$$h_{int,i} = M^{\frac{1}{2}}(\mathcal{R}_{\mathcal{G},i}M^{-\frac{1}{2}})(\dot{\mathcal{R}}_{\mathcal{G},i}v + \mathcal{R}_{\mathcal{G},i}a), \quad i \in \{1,2\}$$

Then $h_{int,1} = h_{int,2}$



The cooperative manipulation system is free of internal forces
if and only if

$$\dot{\mathcal{R}}_{\mathcal{G}}v + \mathcal{R}_{\mathcal{G}}M^{-1}(u - C\dot{v} - g) \in \text{null}(\mathcal{R}_{\mathcal{G}}^T)$$

Cooperative manipulation via internal-force regulation

Association of $G(x)$ and $\mathcal{R}_{\mathcal{E}}(x)$

Theorem 1.

Let N agents rigidly grasping an object, associated with a grasp matrix $G(x)$. Let also the agents be modelled by a complete graph associated with a rigidity matrix $\mathcal{R}_{\mathcal{E}}(x)$

Then

$$\text{null}(G(x)) = \text{range}(\mathcal{R}_{\mathcal{E}}(x)^{\top})$$

$$\begin{aligned} h_o &= G(x)h \\ v &= G(x)^{\top}v_o \end{aligned}$$

$$\mathcal{R}_{\mathcal{E}}(x) = \begin{bmatrix} \frac{\partial \gamma_{\mathcal{E}}}{\partial p_1} & \frac{\partial \gamma_{\mathcal{E}}}{\partial R_1} & \cdots & \frac{\partial \gamma_{\mathcal{E}}}{\partial p_N} & \frac{\partial \gamma_{\mathcal{E}}}{\partial R_N} \end{bmatrix}$$

Cooperative manipulation via internal-force regulation

Relation between forces h and internal forces h_{int}

Theorem 2.

Let N agents rigidly grasping an object. The agent internal forces h_{int} and forces h are related via

$$h_{int} = (I_{6N} - MG^T(GMG^T)^{-1}G)h$$

As opposed to $h_{int} = (I_{6N} - G^T(GG^T)^{-1}G)h$ found in the literature

Cooperative manipulation via internal-force regulation

Internal-force free distribution of a force to the agents

Theorem 3.

Let N agents rigidly grasping an object. Let a desired force $h_{o,d}$ to be applied to the object, distributed to the agents via $h_d = G^* h_{o,d}$, where G^* is a right inverse of G , i.e., $GG^* = I_6$

Then

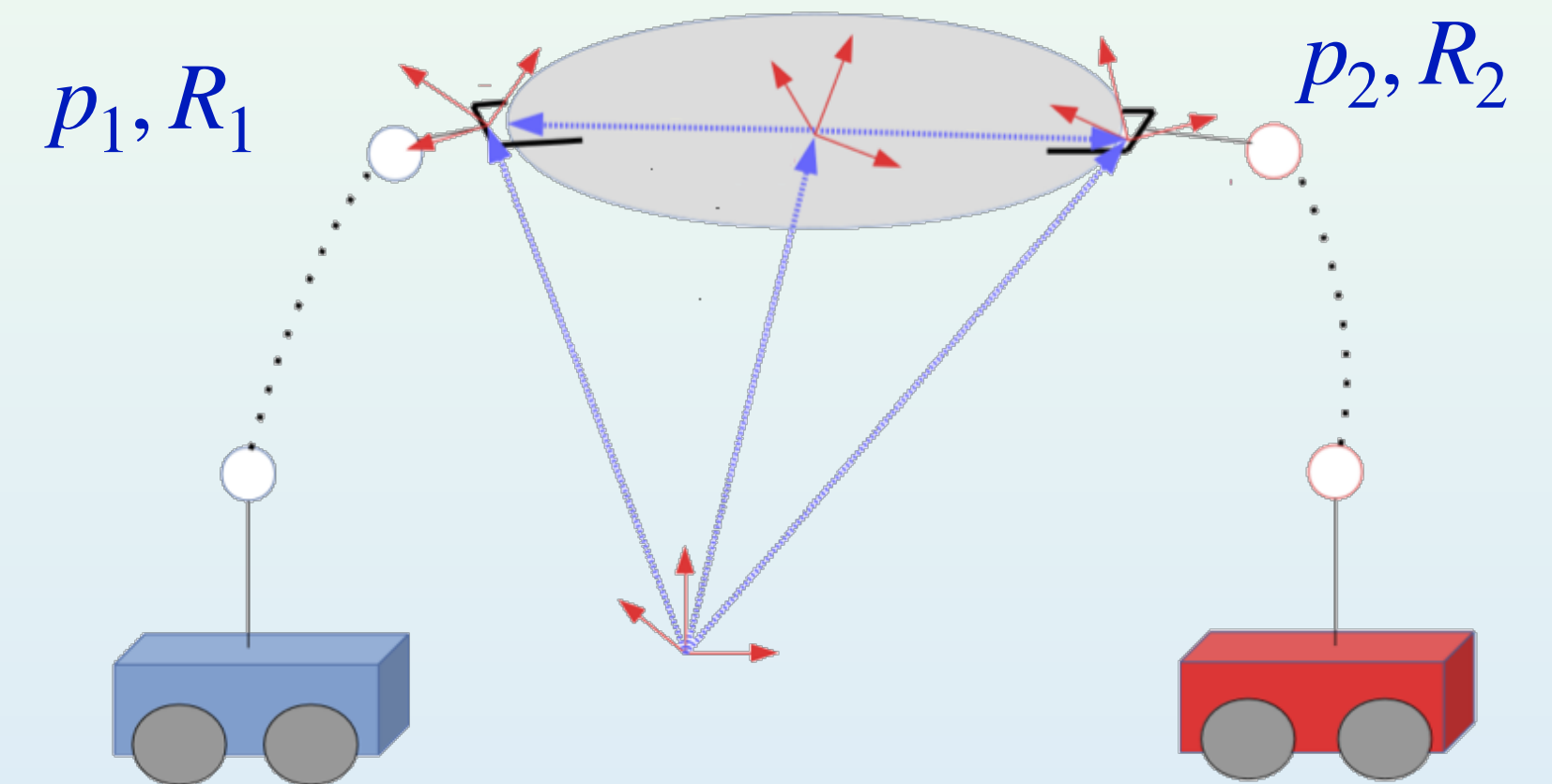
$$h_{int} = 0 \Leftrightarrow G^* = MG^T(GMG^T)^{-1}$$

$$h_o = G(x)h$$

Control design

- Tracking of reference trajectory $\begin{cases} v_d = [\dot{p}_d^\top, \omega_d^\top]^\top \\ \dot{R}_d = S(\omega_d)R_d \end{cases}$

- Associated errors $\begin{cases} e_p = p_o - p_d \\ e_o = \frac{1}{2}\text{tr}(I_3 - R_d^\top R_o) \\ e_R = S^{-1}(R_d^\top R_o - R_o^\top R_d) \\ e_x = \left[e_p^\top, \frac{1}{2(2 - e_o)^2} e_R^\top R_o^\top \right]^\top \\ e_v = v_o - v_d \end{cases}$



- Internal-force-free control law:

$$u = g + (CG^\top + M\dot{G}^\top)v_o + G^*(g_o + C_o v_o) + (MG^\top + G^*M_o)(\dot{v}_d - K_d e_v - K_p e_x)$$

$$h_{int} = 0 \Leftrightarrow G^* = MG^\top (GMG^\top)^{-1}$$

Simulations

- Tracking of reference trajectory

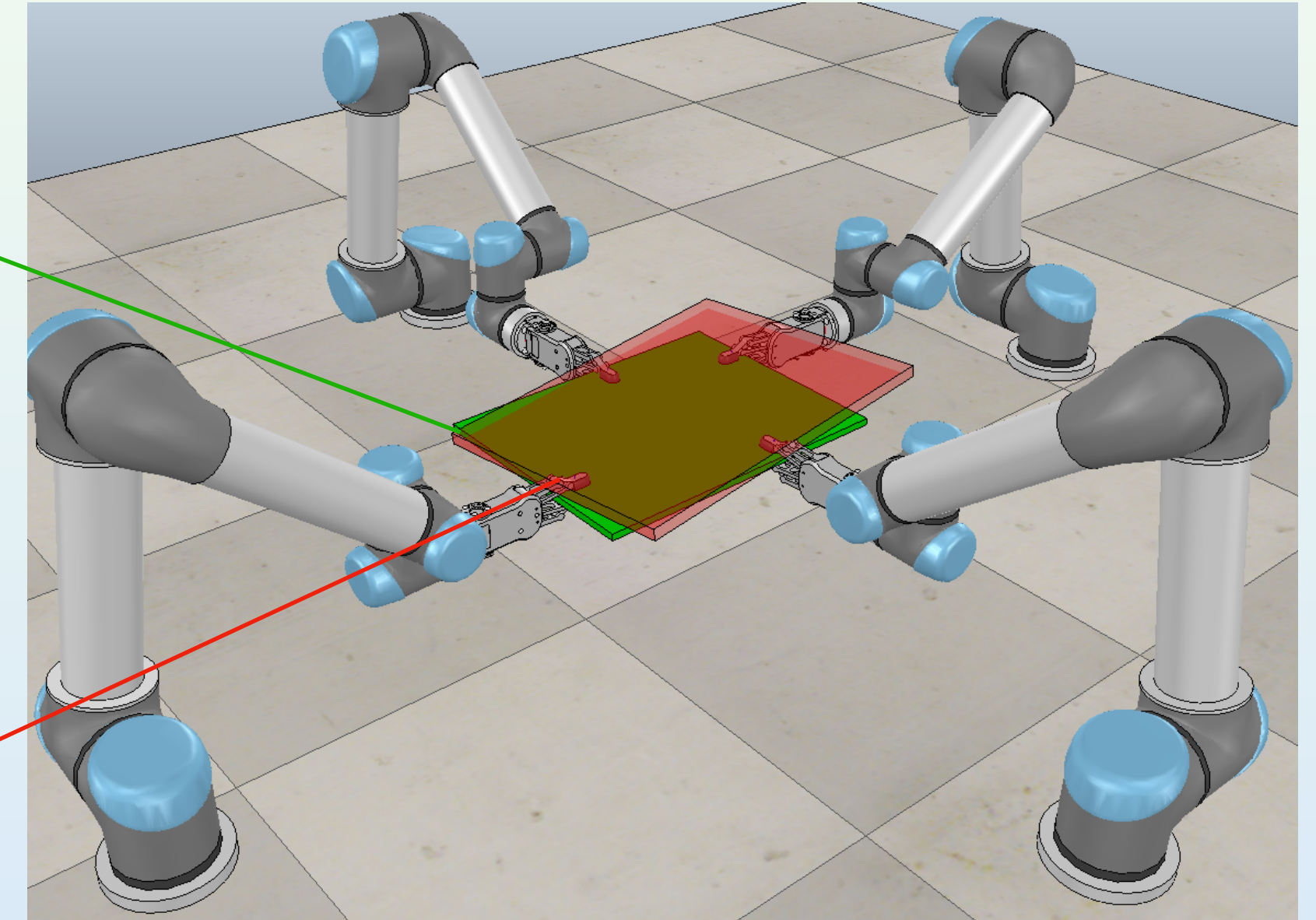
$$p_d(t) = p_o(0) + \begin{bmatrix} 0.2 \sin(t + \frac{\pi}{6}) \\ 0.2 \cos(t + \frac{\pi}{6}) \\ 0.09 + 0.1 \sin(t + \frac{\pi}{6}) \end{bmatrix}$$

$$\eta_d(t) = 0.15 \begin{bmatrix} \sin(t + \frac{\pi}{6}) \\ \sin(0.5t + \frac{\pi}{6}) \\ \sin(t + \frac{\pi}{6}) \end{bmatrix}$$

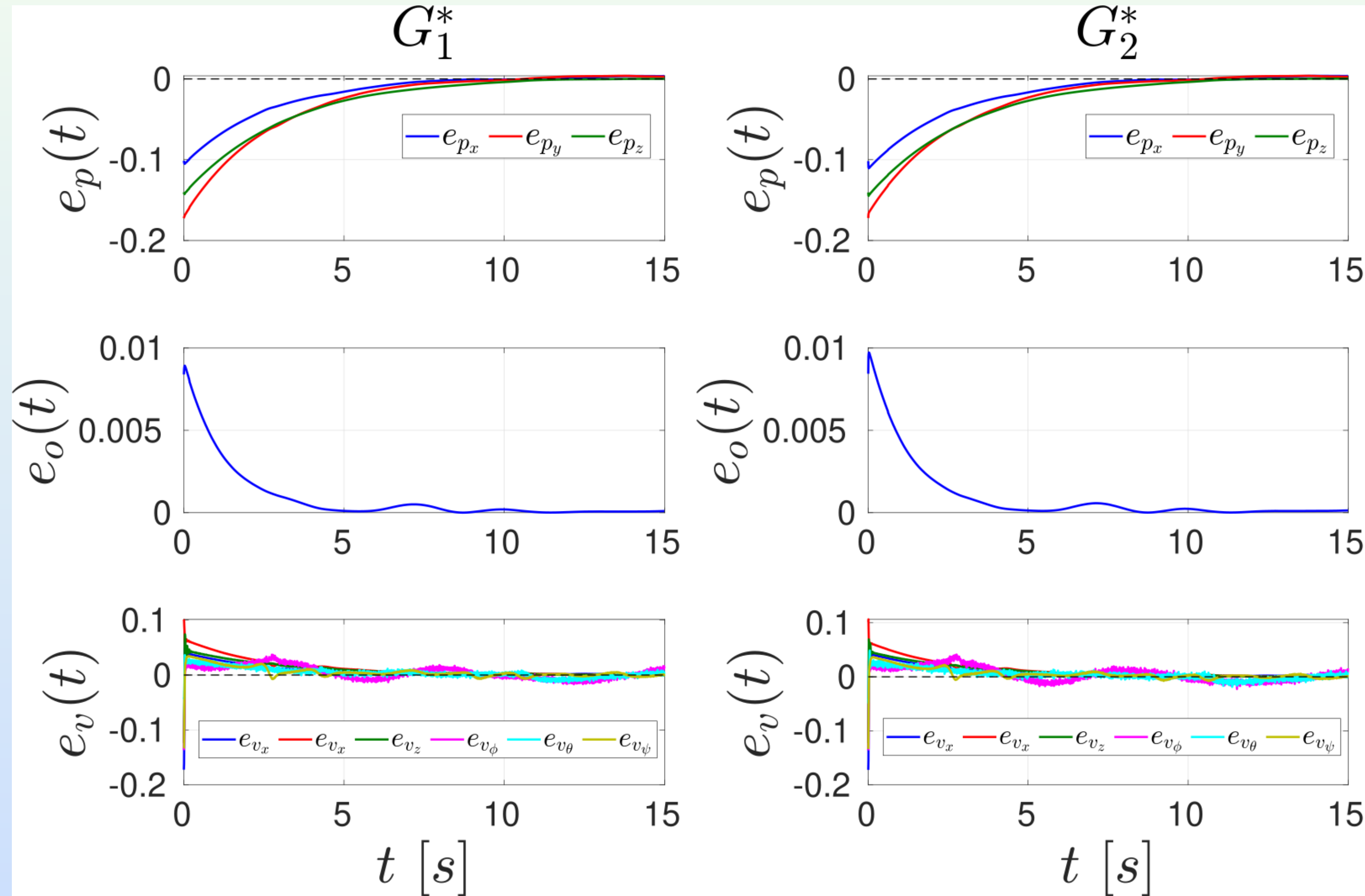
- Comparison among $\begin{cases} G_1^* = MG^T(GMG^T)^{-1} & \text{(proposed)} \\ G_2^* = G^T(GG^T)^{-1} & \text{(related works)} \end{cases}$

object

reference trajectory

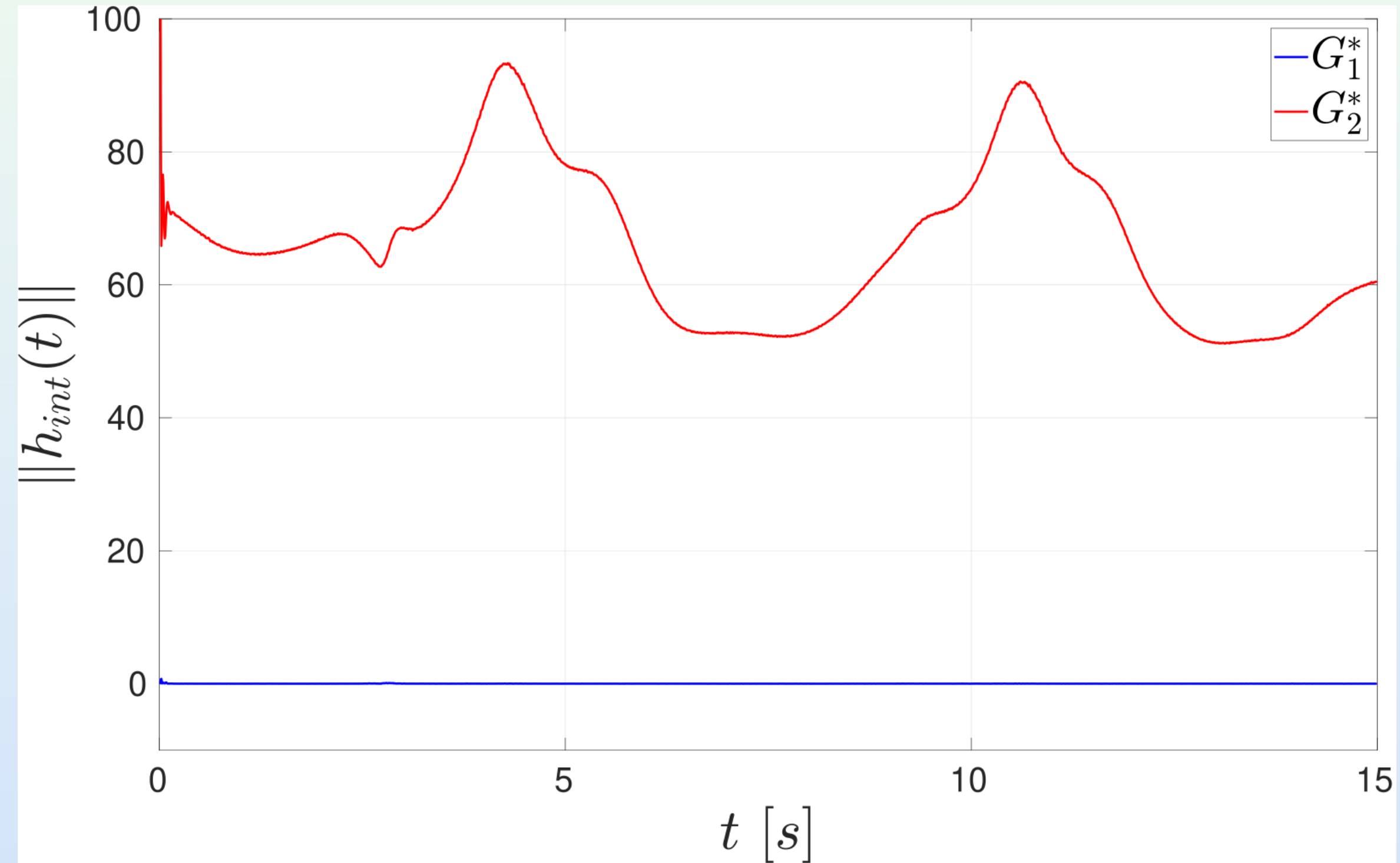


Both schemes achieve tracking

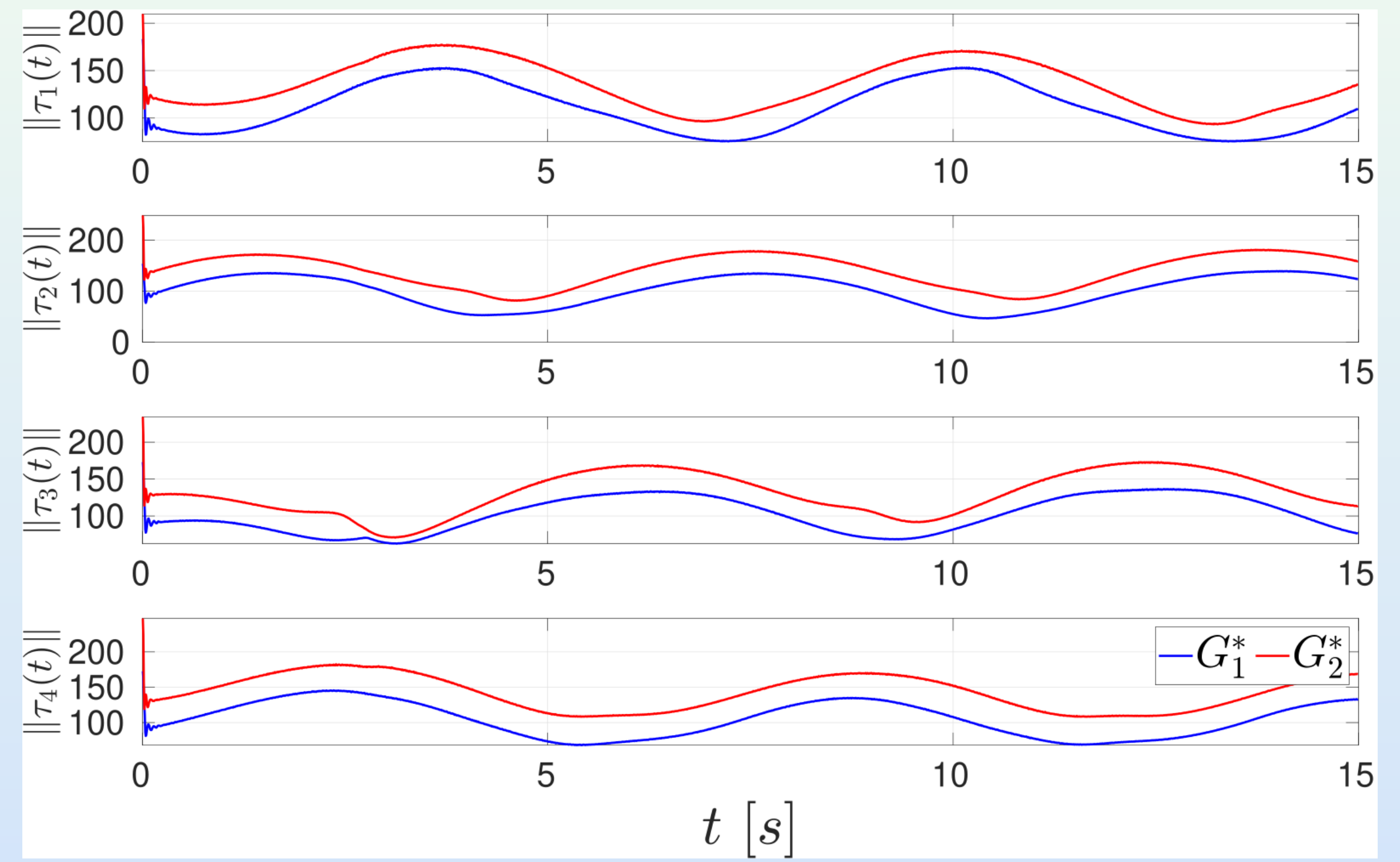


Proposed control achieves zero internal forces

Internal forces



Input norms



Conclusion and future work

Conclusion

- Cooperative manipulation via internal-force regulation
- Association of rigid cooperative manipulation with distance and bearing rigidity
- Control design that guarantees regulation of internal forces

Future work

- Extension to tethered systems
- Decentralisation and dynamic uncertainty