On the Links between Bearing-Rigid Formations and Parallel Robots Application to Singularity Analysis of Rigid Bearing-Based Formations of Quadrotors





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# The importance of rigidity

### Rigidity of frameworks

 "Rigidity theory studies [...] whether two frameworks with the same inter-neighbor bearings have the same shape" [Zhao & Zelazo IEEE TAC 2016]





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### Framework singularities

 "A particular graph will be rigid or flexible in ℝ<sup>n</sup> for almost all locations of its vertices" [Asimow & Roth TAMS 1978]



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Figure: A singularity of a 3-UAV formation



Figure: A singularity of a 4-UAV formation [Pasquetti et al. CORR 2019]

# Singularities of formations

Singularities appearing in the bearing rigidity matrix

• a huge challenge

• Issues with singularities: loss of controllability, of accuracy, impossibility to use pose estimation algorithms nearby



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• Issues with singularities: loss of controllability, of accuracy, impossibility to use pose estimation algorithms nearby

Determining the singularity cases stays an open problem



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The "Hidden Robot Concept": a tool for singularity analysis of rigidity matrices

- A tool made first for visual servoing problems [Briot et al IEEE TRO 2015, Briot et al IEEE TRO 2017]
- Then transferred to the analysis of **singularities of (bearing) rigidity matrices** [Briot & Robuffo Giordano ASME JMR 2019]



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The "Hidden Robot Concept": a tool for singularity analysis of rigidity matrices

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### Basic idea

Intr

- The Inverse Jacobian matrix of a virtual parallel robot  $\Rightarrow$  a basis of the Formation Rigidity Matrix
- Many tools for finding geometric configurations leading to singularities of line systems: Screw Theory [Hunt book 1979], Grassmann geometry [Merlet IJRR 1989], Grassmann-Cayley algebra [Kanaan et al IEEE TRO 2009]

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# A simple graph example







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# A simple graph example







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# A simple graph example



We virtually open the mechanism in  $A_3$  + we fix one prismatic joint to avoid the scaling translation

### Chain $A_2A_1A_3$

• A single twist  $\$_1$  allowed in  $A_3$ :

 $\mathbf{\$}_1 = [\mathbf{p}_{13}^{\mathcal{T}} \, \mathbf{0}]^{\mathcal{T}}$  translation along  $\overrightarrow{A_1 A_3}$ 

As a result, two wrenches constrain ξ<sub>1</sub> and ξ<sub>2</sub> the motion at A<sub>3</sub> (ξ<sup>T</sup><sub>i</sub>\$<sub>1</sub> = 0)

$$\boldsymbol{\xi}_1 = [\mathbf{p}_{13}^{\perp \ T} \ \mathbf{0}]^T$$
 force along  $\overrightarrow{A_1 A_3}^T$ 

 $\boldsymbol{\xi}_2 = [0 \, 0 \, 1]^T$  moment around  $\boldsymbol{z}$ 

# A simple graph example



We virtually open the mechanism in  $A_3$ 

Chain  $A_2A_3$ 

- Two twists  $\$_2$  and  $\$_3$  allowed in  $A_3$ :
  - $\mathbf{\$}_2 = [\mathbf{p}_{23}^T \ \mathbf{0}]^T \text{ translation along } \overrightarrow{A_2 A_3}$ 
    - $\mathbf{\$}_3 = [0 \ 0 \ 1]^T$  rotation around  $\boldsymbol{z}$
- As a result, a single wrench ξ<sub>3</sub> constrains the motion at A<sub>3</sub> (ξ<sub>3</sub><sup>T</sup> \$<sub>j</sub>) = 0)

$$\boldsymbol{\xi}_3 = [\mathbf{p}_{23}^{\perp} \ ^{\mathcal{T}} \ 0]^{\mathcal{T}}$$
 force along  $\overrightarrow{A_2 A_3^{\perp}}$ 

Singularities of quadrotor formations

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# A simple graph example



At the end, mechanism constraint wrench system  $\mathcal{W}$  ( $\equiv$  basis of the rigidity matrix)

$$\mathcal{W} = \begin{bmatrix} \boldsymbol{\xi}_1 \, \boldsymbol{\xi}_2 \, \boldsymbol{\xi}_3 \end{bmatrix}$$
$$= \begin{bmatrix} \mathbf{p}_{13}^{\perp} & \mathbf{p}_{23}^{\perp} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & 1 \end{bmatrix}$$

The system is rigid iff W is full rank rank(W) = 3

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# A simple graph example



At the end, mechanism constraint wrench system  $\mathcal{W}$  ( $\equiv$  basis of the rigidity matrix)

$$\mathcal{W} = [\boldsymbol{\xi}_1 \, \boldsymbol{\xi}_2 \, \boldsymbol{\xi}_3] = egin{bmatrix} \mathbf{p}_{13}^{\perp} & \mathbf{p}_{23}^{\perp} & \mathbf{0} \ \mathbf{0} & \mathbf{0} & \mathbf{1} \end{bmatrix}$$

 $\mathcal{W}$  and **and the rigidity matrix** are singular when locally, rank( $\mathcal{W}$ ) < 3, i.e. when

- **p**<sub>13</sub> is colinear with **p**<sub>23</sub>,
- In other words, when  $A_1$ ,  $A_2$ ,  $A_3$  are aligned.

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### A second graph example







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### A second graph example



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# A second graph example



We virtually open the mechanism in  $A_2$  + we fix one prismatic joint to avoid the scaling translation

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 As a result, a single wrench constrains ξ<sub>1</sub>the motion at A<sub>1</sub> (ξ<sup>T</sup><sub>i</sub>\$<sub>1</sub> = 0)

$$\boldsymbol{\xi}_1 = [\mathbf{p}_{12}^{\perp \ T} \ \mathbf{0}]^T$$
 force along  $\overrightarrow{A_1 A_2^{\perp}}$ 

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# A second graph example



We virtually open the mechanism in  $A_2$  + we fix one prismatic joint to avoid the scaling translation

### Chain $A_3A_1A_2$

• Two twists \$1 and \$2 allowed in A1:

 $\mathbf{\$}_1 = [\mathbf{p}_{12}^T \ \mathbf{0}]^T \text{ translation along } \overrightarrow{A_1 A_2}$  $\mathbf{\$}_2 = [\mathbf{0} \ \mathbf{0} \ \mathbf{1}]^T \text{ rotation around } \mathbf{z}$ 

• or also at  $A_2$ 

$$\boldsymbol{\xi}_1 = [\boldsymbol{\mathsf{p}}_{12}^{\perp \ T} \ (\boldsymbol{\mathsf{p}}_{12}^{\mathsf{T}} \boldsymbol{\mathsf{p}}_{12})]^{\mathsf{T}}$$

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# A second graph example



We virtually open the mechanism in  $A_2$ 

Chain  $A_3A_2$ 

- Two twists  $\$_3$  and  $\$_4$  allowed in  $A_3$ :
  - $\mathbf{\$}_3 = [\mathbf{p}_{32}^T \, \mathbf{0}]^T$  translation along  $\overrightarrow{A_3 A_2}$ 
    - $\mathbf{\$}_4 = [0 \ 0 \ 1]^T$  rotation around  $\boldsymbol{z}$
- As a result, a single wrench ξ<sub>3</sub> constrains the motion at A<sub>3</sub> (ξ<sub>3</sub><sup>T</sup> \$<sub>j</sub>) = 0)

$$oldsymbol{\xi}_2 = [oldsymbol{p}_{23}^{\perp} \, {}^{\mathcal{T}} \, 0]^{\mathcal{T}}$$
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At the end, mechanism constraint wrench system  $\mathcal{W}$  ( $\equiv$  basis of the rigidity matrix)

 $\mathcal{W} = [\boldsymbol{\xi}_1 \, \boldsymbol{\xi}_2]$ 

#### ${\mathcal W}$ is of rank 2:

**One unconstrained motion** (in the nullspace of – or reciprocal to –  $\mathcal{W}$ )

# Hidden Robot and Singularity Analysis

Slides Julian Erskine







The Hidden Robot



# Strategy for a generalized singularity analysis

#### Objectives

- X Analyse all singularities
- Analyse many singularities
- Apply to many formations
- Graph space results

#### What does this do?

- Can we find all  $S^{\mathcal{L}}$ ?
- Can we find all  $\mathcal{S}^{\mathcal{F}}$
- Is  $S^{\mathcal{L}} \cup S^{\mathcal{F}}$  comprehensive?

#### Local analysis

- Apply to each agent  $A_i$
- Assume all agents are fixed



**Figure 5.9** – Local neighbourhood of  $A_i$ 

 $\mathcal{S}^{\mathcal{L}}_{i}$  : Set of embeddings where  $\hat{\mathcal{A}}_{i}$  moves *wrt* others

#### Subformation analysis

- Bi-partition the formation
- Assume one partition fixed



Figure 5.10 – Subformations  ${\cal F}_1$  and  ${\cal F}_2$ 

 $\mathcal{S}^{\mathcal{F}}$  : Set of embeddings where  $\mathcal{F}_1$  moves wrt  $\mathcal{F}_2$ 

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The Hidden Robot



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The Hidden Robot



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### Graph edge primitives

Apply mechanical constraints to graph edges



J. Erskine

PhD Thesis Defence



### Local singularities - two neighbours

#### Building a singularity dictionary

- Find local graph types
- Analyse the 6 hidden robots
- Use set-based analysis (e.g.  $\mathcal{S}_{\mathbb{BO}}^{\mathcal{L}} \supset \mathcal{S}_{\mathbb{BB}}^{\mathcal{L}}$ )



03/12/2021



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Table 3 – Singularities for of  $\mathcal{A}_{\it i}$  connected to agents  $\mathcal{A}_{\it j}$  and  $\mathcal{A}_{\it k}$ 

Туре	Wrenches	Singular Configuration ${\mathcal S}_{\operatorname{type}}^{\mathcal L}$	Singular Twist $\mathcal{T}_{\mathcal{L}type}$
$\mathcal{L}_{\mathbb{BB}}$	$\mathcal{W}_{\mathbb{B}j} \cup \mathcal{W}_{\mathbb{B}k}$	1. $S_{\mathbb{BB}}^{\mathcal{L}}$	1. $\mathcal{T}_{\mathcal{LBB}}$ (see Eq. (??))
$\mathcal{L}_{\mathbb{BO}}$	$\mathcal{W}_{\mathbb{B}j} \cup \mathcal{W}_{\mathbb{O}k}$	1. $S_{\mathbb{BB}}^{\mathcal{L}}$	1. $\mathcal{T}_{\mathcal{LBB}}$
$\mathcal{L}_{\mathbb{BI}}$	$\mathcal{W}_{\mathbb{B}j} \cup \mathcal{W}_{\mathbb{I}k}$	1. $\mathcal{S}_{\mathbb{BB}}^{\mathcal{L}}$ 2. $\mathbf{p}_{ij}$ is vertical	1. $\mathcal{T}_{\mathcal{L}^{\mathbb{BB}}}$ 2. $\mathbf{v}'(\mathbf{z}_0, \mathbf{p}_i)$
$\mathcal{L}_{\mathbb{OI}}$	$\mathcal{W}_{\mathbb{O}j} \cup \mathcal{W}_{\mathbb{I}k}$	1. $\mathcal{S}_{\mathbb{BI}}^{\mathcal{L}}$ 2. $\mathbf{p}_{ij}$ and $\mathbf{p}_{ik}$ are horizontal	$\begin{array}{c} 1. \ \mathcal{T}_{\mathcal{L}\mathbb{BI}} \\ 2. \ \mathbf{v}'(\mathbf{z}_0, \mathbf{c}) \end{array}$
$\mathcal{L}_{\mathbb{OO}}$	$\mathcal{W}_{\mathbb{O}j} \cup \mathcal{W}_{\mathbb{O}k}$	1. $S_{\mathbb{BO}}^{\mathcal{L}}$ 2. $\mathbf{p}_{ij}$ and $\mathbf{p}_{ik}$ are horizontal 3. $\mathbf{p}_{jk}$ is vertical	1. $\mathcal{T}_{\mathcal{L}\mathbb{B}\mathbb{O}}$ 2. $\mathbf{v}^{r}(\mathbf{z}_{0}, \mathbf{c})$ 3. $\mathbf{v}^{r}(\mathbf{z}_{0}, \mathbf{p}_{j})$
$\mathcal{L}_{\mathbb{II}}$	$\mathcal{W}_{\mathbb{I}j} \cup \mathcal{W}_{\mathbb{I}k}$	1. $S_{\mathbb{BI}}^{\mathcal{L}}$ 2. All configurations	1. $\mathcal{T}_{\mathcal{L}\mathbb{BI}}$ 2. $\mathbf{v}'(\mathbf{z}_0, \mathbf{p}_i)$



#### PhD Thesis Defence

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### Local singularities - *n* neighbours

#### Generalization of local analysis

- Infinite number of local hidden robots
- More measurements increases constraints
- There is a closed set of local singularities
- Singularities of all local formations of type  $\mathbb{B}^{a}\mathbb{O}^{b}\mathbb{I}^{c}$  where  $a + b + c \geq 3$ 
  - All edges are co-linear
  - **2** Only  $\mathbb{I}$  edges are non-vertical
- Singularities of local formations of type  $\mathbb{O}^b$ 
  - $\begin{array}{l} \bullet \quad \mathcal{A}_i \text{ and } \mathcal{A}_1 \cdots \mathcal{A}_m \text{ lie on a horizontal circle} \\ \bullet \quad \text{Agents } \mathcal{A}_1 \cdots \mathcal{A}_m \text{ lie on a vertical line.} \end{array}$



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### Subformation singularities - two edges

#### Local analysis is not enough

- Sufficient to imply flexibility
- Insufficient to imply rigidity





#### Subformation singularities

- Assume both subformations are rigid
  - Fix one subformation
  - Other is free in translation, yaw, scale
- Difficult compared to local analysis

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Subformation Singularities



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  - Fix one subformation
  - Other is free in translation, yaw, scale
- Difficult compared to local analysis



Figure 5.20 – Two subformations  $\mathcal{F}_A$  and  $\mathcal{F}_B$  connected by two distinct graph edges

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# Hidden Robot and Singularity Analysis

Table: Classification of all bi-partitioned subformation singularities with two edges

Туре	Singular Configuration $S_{type}^{F}$
$\mathbb{B}\mathbb{B}$	1: Lines $A_1B_1$ and $A_2B_2$ intersect
	2: Lines $A_1B_1$ and $A_2B_2$ are colinear
	3: Lines $A_1B_1$ and $A_2B_2$ are vertical and superposed
BO	1: $\mathcal{S}_{\mathbb{BB}}^{\mathcal{F}}$
	2: Line $A_1B_1$ is vertical and intersects $B_2$

Subformation Singularities



### Subformation singularities - three edges

#### Subformation we can solve

- $\bullet$  Contains  $\mathcal{F}_{_{\mathbb{B}\mathbb{B}}}$  or  $\mathcal{F}_{_{\mathbb{B}\mathbb{O}}}$  as subset
- Can find all singularities

#### Subformation we cannot solve

- $\bullet \ \mathcal{F}_{_{\bigcirc \bigcirc \bigcirc \bigcirc}}$  and  $\mathcal{F}_{_{\mathbb{I} \bigcirc \bigcirc}}$
- Can find some singularities
- Cannot show that there are not others



Figure 5.21 - All three-edge subformations. Prismatic joints containing a circle have coupled twist magnitudes.

# Hidden Robot and Singularity Analysis

Table: Classification of all bi-partitioned subformation singularities with two edges

Туре	Singular Configuration $S_{type}^F$		
BBB	1: All lines $A_i B_i$ intersect 2: All lines $A_i B_i$ are colinear		
	3: All lines $A_i B_i$ vertical, superposed		
OBB	1: $\mathcal{S}_{\mathbb{BBB}}^{\mathcal{F}}$ 2: $B_3$ aligned with $A_1B_1$ , $A_iB_i$ , $i \in 2, 3$ superposed		
OOB	1: $\mathcal{S}_{\mathbb{OBB}}^{\mathcal{F}}$ 2: Line $A_3B_3$ vertical, intersects $B_1$ or $B_2$		
IOB	1: $\mathcal{S}_{\mathbb{OBB}}^{\mathcal{F}}$ 2: Line $A_3B_3$ vertical, intersects $A_1$ and $B_2$		
IOO	1: $\mathcal{S}_{\mathbb{IOB}}^{\mathcal{F}}$ 2: $A_1 B_2 B_3$ aligned and vertical		
	3: All agents $A_i$ , $B_i \forall i$ lie on a common horizontal plane		
000	1: $\mathcal{S}_{\mathbb{OOB}}^{\mathcal{F}}$ 2: $B_i \forall i$ are vertical superposed		
	3: All agents $A_i$ , $B_i \forall i$ lie on a common horizontal plane		
	4: $F_A$ and $F_B$ are bearing-congruent and lie on their common respective horizontal planes.		

# Hidden Robot and Singularity Analysis

### With this analysis

- Able to analyze many singularities in a formation
- Impossible to analyze all singularities for a given arbitrary formation
- BUT possibility to analyze all singularities of properly designed formations
  - simple small sub-formations in which we can easily know all singularities
  - $\circ~$  associated together with 2 or 3 edges in order to form big-sized graphs

ingularities of quadrotor formations

Case study ●0 Conclusions O

# Case studies with 18 drones





ingularities of quadrotor formations

Case study

Conclusions 0

## Case studies with 18 drones



Component	$\#$ of $\mathcal{S}^{L}$	$\#  ext{ of } \mathcal{S}^{\textit{F}}$
$\mathcal{S}_{\mathcal{A}}$	3	
$\mathcal{S}_B$	4	
$\mathcal{S}_{A/B}^{F}$	-	
$\mathcal{S}_{C}$	5	
$\mathcal{S}^{F}_{AB/C}$	-	
$\mathcal{S}_D$	6	
$\mathcal{S}^{F}_{ABC/D}$	-	
Total	18	

•  $\mathcal{F}_A$ : BB, BO, BI

- $\mathcal{F}_B$ :  $\mathbb{BOI} \times 3$ ,  $\mathbb{BBB}$
- $\mathcal{F}_C$ : BOI × 3, OII, BO
- $\mathcal{F}_D^*$ :  $\mathbb{BB} \times 4$ ,  $\mathbb{BO}$ ,  $\mathbb{BI}$

Hidden robot concept: simple examples

ingularities of quadrotor formations

Case study ●0 Conclusions 0

### Case studies with 18 drones



Component	$\#$ of $\mathcal{S}^{L}$	$\#  ext{ of } \mathcal{S}^{\textit{F}}$
$\mathcal{S}_{\mathcal{A}}$	3	0
$\mathcal{S}_B$	4	0
$\mathcal{S}_{A/B}^{F}$	-	
Sc	5	0
$\mathcal{S}^{F}_{AB/C}$	-	
$S_D$	6	1
$\mathcal{S}^{\sf F}_{ABC/D}$	-	
Total	18	

•  $\mathcal{F}_D$ : OII

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### Case studies with 18 drones



Component	$\#$ of $\mathcal{S}^{L}$	$\#  ext{ of } \mathcal{S}^{\textit{F}}$
$\mathcal{S}_{\mathcal{A}}$	3	0
$\mathcal{S}_B$	4	0
$\mathcal{S}_{A/B}^{F}$	-	1
$S_{C}$	5	0
$\mathcal{S}^{F}_{AB/C}$	-	
$S_D$	6	1
$\mathcal{S}^{F}_{ABC/D}$	-	
Total	18	

•  $\mathcal{F}_{AB}$ : OOI

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Case study ●0 Conclusions O

### Case studies with 18 drones



Component	$\#$ of $\mathcal{S}^{L}$	$\#  ext{ of } \mathcal{S}^{\textit{F}}$
$\mathcal{S}_{\mathcal{A}}$	3	0
$\mathcal{S}_B$	4	0
$\mathcal{S}_{A/B}^{F}$	-	1
Sc	5	0
$\mathcal{S}^{\sf F}_{AB/C}$	-	1
$S_D$	6	1
$\mathcal{S}^{\sf F}_{ABC/D}$	-	
Total	18	

•  $\mathcal{F}_{ABC}$ :  $\mathbb{BB}$ 

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### Case studies with 18 drones



Component	$\#$ of $\mathcal{S}^{L}$	$\#  ext{ of } \mathcal{S}^{\textit{F}}$
$\mathcal{S}_{\mathcal{A}}$	3	0
$\mathcal{S}_B$	4	0
$\mathcal{S}_{A/B}^{F}$	-	1
$S_{C}$	5	0
$\mathcal{S}^{F}_{AB/C}$	-	1
$S_D$	6	1
$\mathcal{S}^{\sf F}_{ABC/D}$	-	1
Total	18	4

•  $\mathcal{F}_{ABCD}$ :  $\mathbb{BI}$ 

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### Case studies with 18 drones



65 singularity conditions in total (some of them redundant):

- (1, 2, 3) or (8, 9, 10) or (13, 14, 15) or (13, 14, 15) or (4, 5, 6, 7) or (8, 9, 11, 12) or (9, 10, 11, 12) or (8, 10, 11, 12) *aligned*,
- $\mathbf{p}_{1,3}$  or  $\mathbf{p}_{9,10}$  or  $\mathbf{p}_{14,15}$  or  $(\mathbf{p}_{4,5} \& \mathbf{p}_{4,7})$  or  $(\mathbf{p}_{4,6} \& \mathbf{p}_{5,6})$  or  $(\mathbf{p}_{5,7} \& \mathbf{p}_{6,7})$  or  $(\mathbf{p}_{8,11} \& \mathbf{p}_{8,12})$  or  $(\mathbf{p}_{9,10} \& \mathbf{p}_{10,12})$  or  $(\mathbf{p}_{8,11} \& \mathbf{p}_{8,12})$  vertical
- lines trough (13, 18) & (14, 17) & (15, 16) *intersect* (in at least a point, possibly at infinity)
- ... (other conditions of the same type)
- (2, 3, 4, 5) or (13, 14, 15, 16, 17, 18) in *a common plane*
- ⇒ Possibility to create 65 singularity indices bounded between 0 and 1

### Controller for rigidity maintenance

- Similar to [Zelazo et al RSS 2012] BUT with our singularity conditions
- {0-5} seconds: initial position to singularity position (Case 1)
- After 5 seconds: Use of controller for singularity free maintenance (Case 2)





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• Hi	idden robot: a tool for singulari	ity analysis of rigidity matrices	5	

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Conclusions

# Conclusions

- Hidden robot: a tool for singularity analysis of rigidity matrices
- Problem complexity: not able to find all singularities
  - Many of them
  - $\circ~$  Design fleets for which all singularities are known





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Conclusions

# Conclusions

- Hidden robot: a tool for singularity analysis of rigidity matrices
- Problem complexity: not able to find all singularities
  - Many of them
  - $\circ~$  Design fleets for which all singularities are known
- Controller based on this analysis
  - Behave similarly as existing singularity-avoidance controller
  - BUT we gain an intrinsic comprehension of the physics of the system

